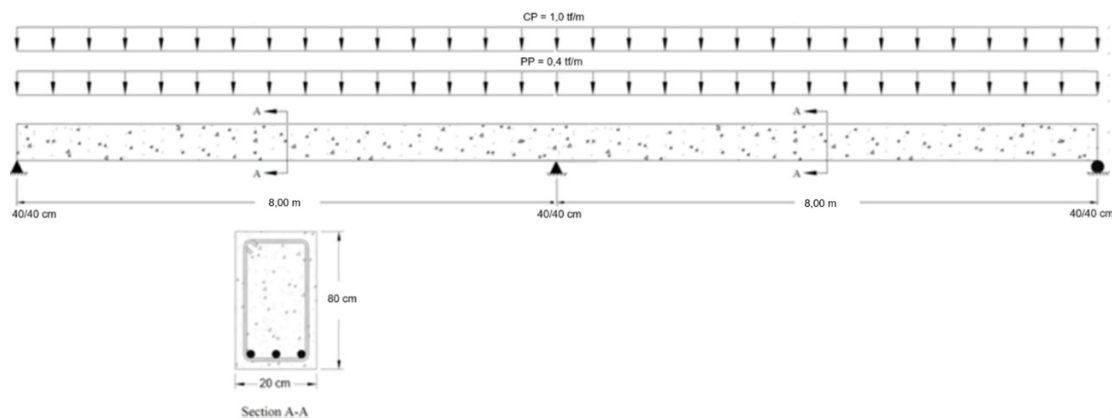


Vigas - Flexão Simples - Viga Continua 6

FLEXÃO SIMPLES

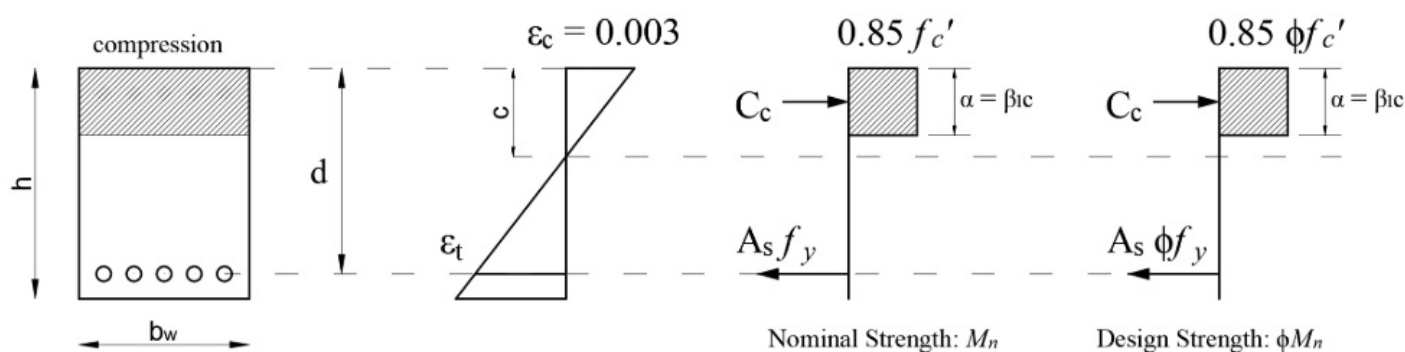
Neste exemplo, será dimensionada a armadura longitudinal e transversal de uma viga submetida a Flexão Simples utilizando como base a Norma ACI318-19, conforme dados abaixo:



Concreto - C25 (4000 psi) / Aço – ADN420 (60 ksi)

b_w : 8 in / h : 31,5 in

TQS	Software B	Software C
Mu+ 619,50 kip.in	Mu+ 597,38 kip.in	Mu+ 690,30 kip.in
Mu- 1185,90 kip.in	Mu- 1202,72 kip.in	Mu- 1197,41 kip.in



Flexão+:

$$M_n = \frac{M_u}{\phi} = \frac{619,50}{0,9} = 688,33 \text{ kip.in}$$

$$d = h - C_c - d_{be} - \frac{d_b}{2} = 31,5 - 1,57 - 0,375 - 0,1875 = 29,37 \text{ in}$$

$$R_n = \frac{M_{n,req}}{b_w \cdot d^2} = \frac{688,33}{8 \cdot 29,37^2} = 0,100 \text{ ksi} = 99,73 \text{ psi}$$

$$\rho = \left(0,85 \cdot \frac{f'_c}{f_y}\right) \cdot \left[1 - \sqrt{1 - \left(\frac{2 \cdot R_n}{0,85 \cdot f'_c}\right)}\right] = \left(0,85 \cdot \frac{4}{60}\right) \cdot \left(1 - \sqrt{1 - \left(\frac{2 \cdot 0,041}{0,85 \cdot 4}\right)}\right) = \mathbf{0,0017}$$

$$A_s = \rho \cdot b_w \cdot d = 0,0017 \cdot 8 \cdot 29,37 = \mathbf{0,43 \text{ in}^2}$$

$A_{s,min}$ (ACI 318-19 – 9.6.1.2)

$$\left(\frac{3 \cdot \sqrt{f'_c}}{f_y}\right) \cdot b_w \cdot d = \left(\frac{3 \cdot \sqrt{4000}}{60000}\right) \cdot 8 \cdot 29,37 = \mathbf{0,74 \text{ in}^2}$$

$$\left(\frac{200}{f_y}\right) \cdot b_w \cdot d = \left(\frac{200}{60000}\right) \cdot 8 \cdot 29,37 = \mathbf{0,78 \text{ in}^2}$$

$$A_{s,req} = A_s \cdot 1,33 = 0,53 \text{ cm}^2 \rightarrow \text{TQS adota adicional devido a altura da viga} \rightarrow \mathbf{0,55 \text{ in}^2}$$

$$\mathbf{A_{s,min} = 0,55 \text{ in}^2}$$

TQS = 0,55 in ²	Software B = 0,52 in ²	Software C = 0,80 in ²
----------------------------	-----------------------------------	-----------------------------------

$$0,55 \text{ in}^2 \geq 0,55 \text{ in}^2 \rightarrow \text{OK!}$$

$$5\#3 \rightarrow 0,55 \text{ in}^2$$

$$\phi M_n (854,35 \text{ kip.in}) \geq M_u (619,50 \text{ kip.in}) \rightarrow \text{OK!!}$$

Verificação do fator de redução (ACI318-19 – 21.2.2)

$$\alpha = \frac{A_s \cdot f_y}{0,85 \cdot f'_c \cdot b_w} = \frac{0,43 \cdot 60}{0,85 \cdot 4 \cdot 8} = 0,87 \text{ in}$$

$$\text{Linha Neutra: } c = \frac{\alpha}{\beta_1} = \frac{0,87}{0,85} = 1,03 \text{ in} \quad c = \frac{\alpha}{\beta_1} = \frac{0,87}{0,85} = 1,03 \text{ in}$$

$$\varepsilon_t = 0,003 \cdot \left(\frac{d - c}{c}\right) = 0,003 \cdot \left(\frac{21,5 - 1,03}{1,03}\right) = \mathbf{0,083}$$

$$0,083 \geq 0,005 \rightarrow \text{OK! Tension Controlled!} \rightarrow \phi 0,90 \text{ OK!}$$

Flexão-:

$$M_n = \frac{M_u}{\phi} = \frac{1185,90}{0,9} = \mathbf{1317,67 \text{ kip.in}}$$

$$d = h - C_c - d_{be} - \frac{d_b}{2} = 31,5 - 1,57 - 0,375 - 0,25 = \mathbf{29,31 \text{ in}}$$

$$R_n = \frac{M_{n,req}}{b_w \cdot d^2} = \frac{1317,67}{8 \cdot 29,31^2} = 0,192 \text{ ksi} = 191,73 \text{ psi}$$

$$\rho = \left(0,85 \cdot \frac{f'_c}{f_y}\right) \cdot \left[1 - \sqrt{1 - \left(\frac{2 \cdot R_n}{0,85 \cdot f'_c}\right)}\right] = \left(0,85 \cdot \frac{4}{60}\right) \cdot \left(1 - \sqrt{1 - \left(\frac{2 \cdot 0,192}{0,85 \cdot 4}\right)}\right) = \mathbf{0,0033}$$

$$A_s = \rho \cdot b_w \cdot d = 0,0033 \cdot 8 \cdot 29,31 = \mathbf{0,77 \text{ in}^2}$$

As,min (ACI 318-19 – 9.6.1.2)

$$\left(\frac{3 \cdot \sqrt{f'_c}}{f_y}\right) \cdot b_w \cdot d = \left(\frac{3 \cdot \sqrt{4000}}{60000}\right) \cdot 8 \cdot 29,31 = \mathbf{0,74 \text{ in}^2}$$

$$\left(\frac{200}{f_y}\right) \cdot b_w \cdot d = \left(\frac{200}{60000}\right) \cdot 8 \cdot 29,31 = \mathbf{0,78 \text{ in}^2}$$

$$\mathbf{A_{s,min} = 0,78 \text{ in}^2}$$

TQS = 0,78 in ²	Software B = 0,79 in ²	Software C = 0,80 in ²
----------------------------	-----------------------------------	-----------------------------------

0,80 in² ≥ 0,78 in² → OK!

4#4 → 0,80 in²

øMn (1228,07 kip.in) ≥ Mu (1185,90 kip.in) → OK!!

Verificação do fator de redução (ACI318-19 – 21.2.2)

$$\alpha = \frac{A_s \cdot f_y}{0,85 \cdot f'_c \cdot b_w} = \frac{0,77 \cdot 60}{0,85 \cdot 4 \cdot 8} = 1,70 \text{ in}$$

$$\text{Linha Neutra: } c = \frac{\alpha}{\beta_1} = \frac{1,70}{0,85} = 2,00 \text{ in}$$

$$\varepsilon_t = 0,003 \cdot \left(\frac{d - c}{c}\right) = 0,003 \cdot \left(\frac{29,31 - 2,00}{2,00}\right) = \mathbf{0,041}$$

0,041 ≥ 0,005 → OK! Tension Controlled! → ø 0,90 OK!

Cortante:

TQS	Software B	Software C
$V_u = 19,65 \text{ kips}$	$V_u = 19,65 \text{ kips}$	$V_u = 19,80 \text{ kips}$
$V_{u,design} = 15,59 \text{ kips}$	$V_{u,design} = 15,72 \text{ kips}$	$V_{u,design} = 15,66 \text{ kips}$

$$V_n = V_c + V_s$$

$$V_u = 19,65 \text{ kips}$$

$$V_{u,design} = 15,59 \text{ kips}$$

$$V_c = 2 \cdot \lambda \cdot \sqrt{f'_c} \cdot b_w \cdot d = 2 \cdot 1 \cdot \sqrt{4000} \cdot 8 \cdot 29,31 = 29,66 \text{ kips}$$

$$V_n = \frac{V_{u,design}}{\phi_{0,75}} = V_c + V_s \rightarrow V_s = 0 \text{ kips} \rightarrow V_n = 20,79 \text{ kips}$$

$$V_{s,lim} = 8 \cdot \sqrt{f'_c} \cdot b_w \cdot d = 8 \cdot \sqrt{4000} \cdot 8 \cdot 29,31 = 118,64 \text{ kips}$$

$V_s \leq V_{s,lim}$ OK!

$\phi_{0,75} \rightarrow \phi V_n \geq V_u \rightarrow 15,59 \geq 15,59 \rightarrow \text{OK!!}$

Área de Aço:

$$A_v = \frac{V_s \cdot s}{f_{yt} \cdot d} = \frac{A_v}{s} = \frac{0}{60 \cdot 29,31} = 0,0 \text{ in}^2$$

$$\frac{A_{v,min}}{s} = \frac{0,75 \cdot \sqrt{f'_c} \cdot b_w}{f_{yt}} = 0,0063 \text{ in}^2$$

$$\frac{A_{v,min}}{s} = \frac{50 \cdot b_w}{f_{yt}} = 0,0067 \text{ in}^2$$

$$A_v \geq A_{v,min} \rightarrow 0,00 \leq 0,0067 \rightarrow A_{v,min}!!$$

Espaçamento:

$$s \leq s_{max} \rightarrow s_{max} = \text{menor valor entre } s_1 \text{ e } s_2$$

$$s_1 = \frac{d}{2} = 14,7 \text{ in ou } s_2 = 24 \text{ in} \rightarrow 14,7 \text{ in!} \rightarrow 10 \text{ in!!}$$

$$\phi_t = \#3 \rightarrow \#3 @ 10 \text{ in}$$

$$\phi V_n (51,37 \text{ kips}) \geq V_u (15,59 \text{ kips})$$